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In the Specification:

Rewrite the paragraph at page 5, line 8 as follows.

Turning now to FIG. 2, there is a block diagram showing signal flow in an STTD encoder of the present invention that may be used with the transmitter of FIG. 1. The STTD encoder receives symbol S_1 at symbol time T and symbol S_2 at symbol time $2T$ on lead 200. The STTD encoder produces symbol S_1 on lead 204 and symbol $-S_2^*$ on lead 206 at symbol time T , where the asterisk indicates a complex conjugate operation. Furthermore, the symbol time indicates a relative position within a transmit frame and not an absolute time. The STTD encoder then produces symbol S_{12} on lead 204 and symbol S_1^* on lead 206 at symbol time $2T$. The bit or chip signals of these symbols are transmitted serially along respective paths 208 and 210. Rayleigh fading parameters are determined from channel estimates of pilot symbols transmitted from respective antennas at leads 204 and 208. For simplicity of analysis, a Rayleigh fading parameter α_j^1 is assumed for a signal transmitted from the first antenna 204 along the j^{th} path. Likewise, a Rayleigh fading parameter α_j^2 is assumed for a signal transmitted from the second antenna 206 along the j^{th} path. Each i^{th} chip or bit signal $r_j(i + \tau_j)$ of a respective symbol is subsequently received at a remote mobile antenna 212 after a transmit time τ_j corresponding to the j^{th} path. The signals propagate to a despreader input circuit (FIG. 6) where they are summed over each respective symbol time to produce output signals R_j^1 and R_j^2 corresponding to the j^{th} of L multiple signal paths as previously described.

Rewrite the paragraph at page 6, line 4 as follows.

Referring now to FIG. 3, there is a schematic diagram of a phase correction circuit of the present invention that may be used with a remote mobile receiver. This phase correction circuit receives signals R_j^1 and R_j^2 as input signals on leads 610 and 614 as shown in equations [5-6], respectively.

$$R_j^1 = \sum_{i=0}^{N-1} r_j(i + \tau_j) = \alpha_j^1 S_1 - \alpha_j^2 S_2^* \quad [5]$$

$$R_j^2 = \sum_{i=N}^{2N-1} r_j(i + \tau_j) = \alpha_j^1 S_{12} + \alpha_j^2 S_1^* \quad [6]$$

The phase correction circuit receives a complex conjugate of a channel estimate of a Rayleigh fading parameter α_j^1 corresponding to the first antenna on lead 302 and a channel estimate of another Rayleigh fading parameter α_j^2 corresponding to the second antenna on lead 306. Complex conjugates of the input signals are produced by circuits 308 and 330 at leads 310 and 322, respectively. These input signals and their complex conjugates are multiplied by Rayleigh fading parameter estimate signals and summed as indicated to produce path-specific first and second symbol estimates at respective output leads 318 and 322 as in equations [7-8].